Amendments to the Specification

Please replace the paragraph beginning on page 7, line 35, through page 8, line 7, with the following rewritten paragraph:

In the examples described below, it is assumed that a signal frequency is 1 MHz band, a frequency of noises to be removed is 10 to 500 MHz band, and that the X-R cross-point frequency to discriminate between the signal frequency and the noise frequency is from 10 MHz downward, and resistivity ρ, which is to be determined by a voltage applied to a cable, such as a signal line and a power line, is set at 150 Ωm which falls within a range where problems are kept off at an anticipated voltage in normal applications. Under the aforementioned assumption, basic component compositions are set so that the real part ε' of the complex relative permittivity of a soft magnetic material ranges from 1,000 up to ~~2,000~~ 20,000 at 1 kHz, and from 50 downward at 1 MHz.

Please replace the paragraph beginning on page 8, line 34, through page 9, line 12, with the following rewritten paragraph:

Sample 2 has a basic component composition as shown by S2 in Fig. 2, specifically 47. 0 mol % Fe_2O_3, ~~10.5~~ 11.5 mol % ZnO, 0.5 mol % SnO_2, 1.5 mol % CuO, and 39.5 mol % MnO, which falls within a proposed material composition of 44.0 to 50.0 (50.0 excluded) mol % Fe_2O_3, 4.0 to 26.5 mol % ZnO, 0.1 to 8.0 mol % at least one of TiO_2 and SnO_2, 0.1 to 16.0 mol % CuO, and the rest consisting of MnO. Material powders Fe_2O_3, ZnO, SnO_2, CuO, and MnO as main components pre-weighed for a predetermined ratio as shown by S2 in Fig. 2 were mixed by a ball mill to produce a mixture, and the mixture was calcined at 900 degrees C for 2 hours in the atmosphere. The mixture calcined was pulverized by a ball mill into particles with a grain diameter averaging about 1.4 μm. Then, the mixture pulverized was

mixed with polyvinyl alcohol added, was granulated, and press-molded under a pressure of 80 MPa into a green compact of a toroidal magnetic core with a post-sinter dimension of 15 mm in outer diameter, 8 mm in inner diameter, and 3 mm in height. The green compact was sintered at 1,150 degrees C for 3 hours in an atmosphere with its oxygen partial pressure controlled by pouring in nitrogen.

Please replace the paragraph beginning on page 10, line 11, through line 17, with the following rewritten paragraph:

Referring to Fig. 4, Samples 1 and 2 have the real parts ε' of complex relative permittivity measuring over 10,000 at 1 kHz, but decreasing at 5 kHz upward and measuring about 30 at 1 MHz. Sample 3 of general Mn-Zn-based ferrite has the real part ε' of complex relative permittivity measuring over 100,000 at 1 kHz, about ~~2,000~~ 20,000 at 1 MHz, and still over 1,000 at 10 MHz. And, Sample 4 of Ni-Zn-based ferrite has the real part ε' of complex relative permittivity measuring as low as about 20 even at 1 kHz.

Please replace the paragraph beginning on page 10, line 18, through line 26, with the following rewritten paragraph:

Referring to Fig. 5 where the abscissa axis represents frequency, and the ordinate axis represents impedance, Sample 3 has its impedance characteristic significantly deteriorating compared with the other samples in a frequency band from 10 MHz upward, that is a frequency range crucial to anti-noise measures in the examples of the present invention where it is assumed that a signal frequency is 1 MHz band, and a noise frequency is 10 to 500 MHz band. This happens because Mn-Zn-based ferrite for Sample 3 has a low resistivity ρv, and

also has the real part ε' of complex relative permittivity measuring over 100,000 at 1 kHz, about ~~2,000~~ 20,000 at 1 MHz, and still over 1,000 at 10 MHz.

Please replace the Abstract with the attached amended Abstract.